



| ECP Helical Piles, Tiebacks & Anchors | | Ultimate Capacity Based Upon Torque (kips - kN) (1) (2) | Helix Bearing Plate Grade & Thickness (in - mm) | Section Coupling Method | Building Code Certifications |
|--|---|--|--|--|---------------------------------|
| Rou | und Corner Square Bar (RCS) | | | | |
| Model TAF-150 | 1.50 in - 38.1 mm C1530, Yield Strength = 90 ksi (min) | Comp = 70 kips - 311 kN Ten = 70 kips - 311 kN | ASTM A572 Grade 50 0.375 in - 9.5 mm std 0.50 in - 12.7 mm opt | (1) 0.75 in - 19.1 mm Grd 8 Bolt | ESR 3559 |
| Model TAF-175 | 1.75 in - 44.5 mm C1530, Yield Strength = 90 ksi (min) | Comp = 100 kips - 445 kN Ten = 100 kips - 445 kN | ASTM A572 Grade 50 std 0.375 in - 9.5 mm std 0.50 in - 12.7 mm opt | (1) 0.75 in - 19.1 mm Grd 8 Bolt | ESR 3559 |
| Model TAF-200 | 2.00 in - 50.8 mm C1530, Yield Strength = 90 ksi (min) | Comp = 150 kips - 667 kN Ten = 150 kips - 667 kN | ASTM A572 Grade 80 std .50 in - 12.7 mm std | (1) 0.75 in - 19.1 mm Grd 8 Bolt | none |
| Model TAF-225 | 2.25 in - 57.2 mm C1530, Yield Strength = 90 ksi (min) | Comp = 200 kips - 890 kN Ten = 200 kips - 890 kN | ASTM A572 Grade 80 std 0.50 in - 12.7 mm std | (2) 0.75 in - 19.1 mm Grd 8 Bolts | none |
| | Square Tube | | | | |
| Model HTAF-30S | 3.00 in - 76.2 mm 0.3125 in - 7.94 mm Wall | Comp = 150 kips - 1068 kN Ten = 150 kips - 1068 kN | ASTM A572 Grade 80 std 0.50 in - 12.7 mm std | (1) 0.875 in - 22.2 mm Grade 8 Bolt | none |
| Round Shaft | | | | | |
| Model TAF-288L | O.D. = 2.875 in - 73.0 mm Wall = 0.203 in - 5.2 mm ASTM A500 Grade B or C Yield Strength = 60 ksi (min) | Comp = 44 kips - 196 kN Ten = 44 kips - 196 kN | ASTM A572 Grade 50 0.375 in - 9.5 std 0.50 in - 12.7 opt | (2) 0.75 in - 19.1 mm Grd 8 Bolts | none |
| Model TAF-288 | O.D. = 2.875 in - 73.0 mm Wall = 0.262 in - 6.7 mm ASTM A500 Grade B or C Yield Strength = 60 ksi (min) | Comp = 80 kips - 356 kN Ten = 80 kips - 356 kN | ASTM A572 Grade 50 0.375 in - 9.5 std 0.50 in - 12.7 mm opt | (3) 0.75 in - 19.1 mm Grd 8 Bolts | ESR 3559 |
| Model TAF-288H | O.D. = 2.875 in - 73.0 mm Wall = 0.262 in - 6.7 mm HRPOSLA Grade H490SI Yield Strength = 81 ksi (min) | Comp = 100 kips - 445 kN Ten = 100 kips - 445 kN | ASTM A572 Grade 50 0.375 in - 9.5 std 0.50 in - 12.7 mm opt | (3) 0.75 in - 19.1 mm Grd 8 Bolts | none |
| Model TAF-350 | O.D. = 3.50 in - 88.9 mm Wall = 0.300 in - 7.6 mm ASTM A500 Grade B or C Yield Strength = 60 ksi (min) | Comp = 115 kips - 512 kN Ten = 120 kips - 512 kN | ASTM A572 Grade 50 0.375 in - 9.5 std 0.50 in - 12.7 mm opt | (3) 1.00 in - 25.4 mm Grd 8 Bolts | ESR 3559 |
| Model TAF-450 | O.D. = 4.50 in - 114.3 mm Wall = 0.337 in - 8.6 mm ASTM A500 Grade B or C Yield Strength = 50 ksi (min) | Comp = 160 kips - 712 kN Ten = 160 kips - 712 kN | ASTM A572 Grade 50 0.375 in - 9.5 mm std 0.50 in - 12.7 mm opt | (3) 1.25 in - 28.6 mm Grd 8 Bolts | none |
| Model MTAH-55E | O.D. = 5.50 in - 139.7 mm Wall = 0.375 in - 9.53 mm | Comp = 240 kips - 1068 kN Ten = 240 kips - 1068 kN | ASTM A572 Grade 50 0.75 in - 19.05 mm std | (3) 1.25 in - 28.6 mm Grd 8 Bolts | none |
| Model TAF-663 | O.D. = 6.625 in - 168.3 mm Wall = 0.280 in - 7.1 mm ASTM A500 Grade B or C Yield Strength = 50 ksi (min) | Comp = 200 kips - 890 kN Ten = 200 kips - 890 kN | ASTM A572 Grade 50 0.50 in - 12.7 mm opt 0.75 in - 18.04 mm opt | Weld or Bolt | none |





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|---------------------------------------|---|--|---|--------------------------------------|---------------------------------|
| Model MTAH-70E | O.D. = 6.625 in - 168.3 mm Wall = 0.432 in - 10.97 mm | Comp = 328 kips - 1459 kN Ten = 328 kips - 1459 kN | ASTM A572 Grade 50 0.75 in - 19.05 mm std | (3) 1.25 in - 28.6 mm Grd 8 Bolts | none |
| Model TAF-863 | O.D. = 8.625 in - 219.1 mm Wall = 0.250 in - 6.4 mm ASTM A500 Grade B or C Yield Strength = 50 ksi (min) | Comp = 300 kips - 1335 kN Ten = 300 kips - 1335 kN | ASTM A572 Grade 50 0.50 in - 12.7 mm opt 0.75 in - 18.04 mm opt | Weld or Bolt | none |

⁽¹⁾ The values shown only address torque correlated soil capacity. Other mechanical limit states of the pile/anchor, its couplers, and its connections to the structure (brackets) may also govern the design capacity. Refer to the manufacturer's technical manual for further information."

⁽²⁾ Large diameter helical piles develop capacity by a combination of both end-bearing and skin friction. The ultimate pile capacity is calculated based on the site-specific soil profile on a case-by-case basis. Load tests are often recommended for larger shaft sizes to identify a site-specific torque correlation factor (Kt), to determine the pile displacement versus load, and to verify the helical pile configuration.